

Chapter 6

(AST301) Design and Analysis of Experiments II

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Lecture Outline

1 6. The 2^k Factorial Design

- 6.1 Introduction
- 6.2 The 2^2 design
- 6.3 The 2^3 design
- 6.4 The general 2^k design
- 6.5 A single replicate of the 2^k design
- 6.6 Additional Examples of Unreplicated 2^k Designs
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- 6.8 The Addition of Center Points to the 2^k Design

Section 1

6. The 2^k Factorial Design

Subsection 1

6.1 Introduction

6.1 Introduction

- Factorial designs are widely used in experiments involving several factors where it is necessary to study the joint effect of the factors on a response.
- Chapter 5 presented general methods for the analysis of factorial designs.
- However, several special cases of the general factorial design are important because they are widely used in research work and also because they form the basis of other designs of considerable practical value.

6.1 Introduction

- The most important of these special cases is that of k factors, each at only two levels.
- These levels may be **quantitative**, such as two values of temperature, pressure, or time; or they may be **qualitative**, such as two machines, two operators, the “high” and “low” levels of a factor, or perhaps the presence and absence of a factor.
- A complete replicate of such a design requires $2 \times 2 \times \cdots \times 2 = 2^k$ observations and is called a 2^k **factorial design**.
- This chapter focuses on this extremely important class of designs. Throughout this chapter, we assume that
 - ① the factors are fixed,
 - ② the designs are completely randomized, and
 - ③ the usual normality assumptions are satisfied.

6.1 Introduction

The 2^k design is particularly useful in the early stages of experimental work when many factors are likely to be investigated.

It provides the smallest number of runs with which k factors can be studied in a complete factorial design.

Consequently, these designs are widely used in **factor screening experiments** (where the experiments is intended in discovering the set of **active** factors from a large group of factors).

Subsection 2

6.2 The 2^2 design

6.2 The 2^2 design

- The first design in the 2^k series is one with only two factors, say A and B , each run at two levels.
- This design is called a 2^2 **factorial design**.
- The levels of the factors may be arbitrarily called “low” and “high.”

6.2 The 2^2 design

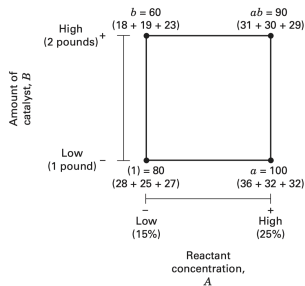
- Consider an investigation into the effect of the concentration of the reactant (factor A) and the amount of catalyst (factor B) on the yield in a chemical process.
 - ▶ Levels of factor A: 15 and 25 percent
 - ▶ Levels of factor B: 1 and 2 pounds
- The objective of the experiment is to determine if adjustments to either of these two factors would increase the yield.
- The experiment is replicated three times, so there are 12 runs. The order in which the runs are made is random, so this is a **completely randomized experiment**.

6.2 The 2^2 design

Data layout:

Factor		Treatment combination	Replicate			Total	Notation
A	B		I	II	III		
-	-	A low, B low	28	25	27	80	(1)
+	-	A high, B low	36	32	32	100	<i>a</i>
-	+	A low, B high	18	19	23	60	<i>b</i>
+	+	A high, B high	31	30	29	90	<i>ab</i>

Graphical view:



6.2 The 2^2 design

By convention, we denote the effect of a factor by a capital Latin letter.

- “A” refers to the effect of factor A,
- “B” refers to the effect of factor B, and
- “AB” refers to the AB interaction.
- The four treatment combinations in the design are represented by lowercase letters.

6.2 The 2^2 design

- The high level of any factor in the treatment combination is denoted by the corresponding lowercase letter and that the low level of a factor in the treatment combination is denoted by the absence of the corresponding letter.
- Thus a represents the treatment combination of A at the high level and B at the low level, b represents A at the low level and B at the high level, and ab represents both factors at the high level.
- By convention, (1) is used to denote both factors at the low level.
- This notation is used throughout the 2^k series.

6.2 The 2^2 design

- In a two-level factorial design the average effect of a factor is defined as the change in response produced by a change in the level of that factor averaged over the levels of the other factor.
- The symbols (1) , a , b , and ab represent the *total* of the response observation at all n replicates taken at the treatment combination.
- The effect of A at the low level of B is $[a - (1)]/n$, and the effect of A at the high level of B is $[ab - b]/n$. Averaging these two quantities yields the *main effect* of A :

$$\begin{aligned} A &= \frac{1}{2} \left\{ \frac{[ab - b] + [a - (1)]}{n} \right\} \\ &= \frac{1}{2n} [ab + a - b - (1)] \end{aligned}$$

6.2 The 2^2 design

- The main effect of B is:

$$\begin{aligned} B &= \frac{1}{2} \left\{ \frac{[ab - a] + [b - (1)]}{n} \right\} \\ &= \frac{1}{2n} [ab + b - a - (1)] \end{aligned}$$

- We define the **interaction effect** AB as the average difference between the effect of A at the high level of B and the effect of A at the low level of B . Thus,

$$\begin{aligned} AB &= \frac{1}{2} \left\{ \frac{[ab - b] - [a - (1)]}{n} \right\} \\ &= \frac{1}{2n} [ab + (1) - a - b] \end{aligned} \quad (6.3)$$

- Alternatively, we may define AB as the average difference between the effect of B at the high level of A and the effect of B at the low level of A . This will also lead to Equation 6.3.

6.2 The 2^2 design

$$A = \frac{1}{2(3)}(90 + 100 - 60 - 80) = 8.33$$

$$B = \frac{1}{2(3)}(90 + 60 - 100 - 80) = -5.00$$

$$AB = \frac{1}{2(3)}(90 + 80 - 100 - 60) = 1.67$$

6.2 The 2^2 design

- The effect of A (reactant concentration) is positive; this suggests that increasing A from the low level (15%) to the high level (25%) will increase the yield.
- The effect of B (catalyst) is negative; this suggests that increasing the amount of catalyst added to the process will decrease the yield.
- The interaction effect appears to be small relative to the two main effects.

The **magnitude** and **direction** of factor effects can be used to determine the important factor and **ANOVA** can generally be used to confirm the interpretation.*

Sum of squares

- Now we consider determining the sums of squares for A , B , and AB .
- Note that, in estimating A , a **contrast** is used:

$$A = \frac{1}{2n}[ab + a - b - (1)] = \left(\frac{1}{2n}\right) \text{Contrast}_A$$

Similarly,

$$B = \frac{1}{2n}[ab - a + b - (1)] = \left(\frac{1}{2n}\right) \text{Contrast}_B$$

$$AB = \frac{1}{2n}[ab - a - b + (1)] = \left(\frac{1}{2n}\right) \text{Contrast}_{AB}$$

- The three contrasts — Contrast_A , Contrast_B , and Contrast_{AB} — are **orthogonal**.

Sum of squares

The sum of squares for any contrast is equal to *the contrast squared* divided by *the number of observations in each total in the contrast* times *the sum of the squares of the contrast coefficients*.

$$SS_A = \left(\frac{1}{2^2 n} \right) \text{Contrast}_A^2 = \frac{1}{4n} [ab + a - b - (1)]^2$$

Sum of squares

$$SS_A = \left(\frac{1}{2^2 n}\right) \text{Contrast}_A^2 = \frac{1}{4n} [ab + a - b - (1)]^2$$

$$SS_B = \left(\frac{1}{2^2 n}\right) \text{Contrast}_B^2 = \frac{1}{4n} [ab - a + b - (1)]^2$$

$$SS_{AB} = \left(\frac{1}{2^2 n}\right) \text{Contrast}_{AB}^2 = \frac{1}{4n} [ab - a - b + (1)]^2$$

Total sum of squares

$$SS_T = \sum_i \sum_j \sum_k y_{ijk}^2 - \frac{y_{...}^2}{4n}$$

Error sum of square

$$SS_E = SS_T - SS_A - SS_B - SS_{AB}$$

Sum of squares

$$SS_A = \left(\frac{1}{2^2 n}\right) \text{Contrast}_A^2 = \frac{1}{4n} [ab + a - b - (1)]^2 = 208.333$$

$$SS_B = \left(\frac{1}{2^2 n}\right) \text{Contrast}_B^2 = \frac{1}{4n} [ab - a + b - (1)]^2 = 75$$

$$SS_{AB} = \left(\frac{1}{2^2 n}\right) \text{Contrast}_{AB}^2 = \frac{1}{4n} [ab - a - b + (1)]^2 = 8.333$$

Total sum of squares

$$SS_T = \sum_i \sum_j \sum_k y_{ijk}^2 - \frac{y_{\dots}^2}{4n} = 323$$

Error sum of square

$$SS_E = SS_T - SS_A - SS_B - SS_{AB} = 31.333$$

Analysis of Variance table

■ **TABLE 6.1**

Analysis of Variance for the Experiment in Figure 6.1

Source of Variation	Sum of Squares	Degrees of Freedom	Mean Square	F_q	P -Value
<i>A</i>	208.33	1	208.33	53.15	0.0001
<i>B</i>	75.00	1	75.00	19.13	0.0024
<i>AB</i>	8.33	1	8.33	2.13	0.1826
Error	31.34	8	3.92		
Total	323.00	11			

- On the basis of the p-values, we conclude that the main effects are statistically significant and that there is no interaction between these factors. This confirms our initial interpretation of the data based on the magnitudes of the factor effects.

Standard order of treatment combinations

- Treatment combinations written in the order $(1), a, b, ab$ is known as **standard order** or Yates' order.
- Using this standard order, we see that the contrast coefficients used in estimating the effects are

Effects	(1)	<i>a</i>	<i>b</i>	<i>ab</i>
<i>A</i>	-1	+1	-1	+1
<i>B</i>	-1	-1	+1	+1
<i>AB</i>	+1	-1	-1	+1

- Note that the contrast coefficients for estimating the interaction effect are just the product of the corresponding coefficients for the two main effects.

Algebraic signs for calculating effects in 2^2 design

- The contrast coefficient is always either $+1$ or -1 , and a **table of plus and minus signs** such as in Table 6.2 can be used to determine the proper sign for each treatment combination

■ TABLE 6.2

Algebraic Signs for Calculating Effects in the 2^2 Design

Treatment Combination	Factorial Effect			
	<i>I</i>	<i>A</i>	<i>B</i>	<i>AB</i>
(1)	+	-	-	+
<i>a</i>	+	+	-	-
<i>b</i>	+	-	+	-
<i>ab</i>	+	+	+	+

- The symbol “*I*” indicates the total or average of the entire experiment.
- To find the contrast for estimating any effect, simply multiply the signs in the appropriate column of the table by the corresponding treatment combination and add.
 - For example, to estimate *A*, the contrast is $-(1) + a - b + ab$.

Algebraic signs for calculating effects in 2^2 design

- The contrasts for the effects A , B , and AB are orthogonal. Thus, the 2^2 (and all 2^k designs) is an orthogonal design.
- The ± 1 coding for the low and high levels of the factors is often called the **orthogonal coding** or the **effects coding**.

Regression model

- In a 2^k factorial design, it is easy to express the results of the experiment in terms of a regression model.
- For the chemical process experiment, the regression model is

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \epsilon,$$

where

- ▶ x_1 and x_2 are the **coded variables** for the reactant concentration and the amount of catalyst, respectively
- ▶ β 's are regression coefficients

Regression model

The relationship between the **natural variables**, the reactant concentration and the amount of catalyst, and the coded variables is

$$x_1 = \frac{\text{Conc} - (\text{Conc}_{\text{low}} + \text{Conc}_{\text{high}})/2}{(\text{Conc}_{\text{high}} - \text{Conc}_{\text{low}})/2}$$

$$x_2 = \frac{\text{Catalyst} - (\text{Catalyst}_{\text{low}} + \text{Catalyst}_{\text{high}})/2}{(\text{Catalyst}_{\text{high}} - \text{Catalyst}_{\text{low}})/2}$$

Regression model

The coded variables are defined as

$$\begin{aligned}x_1 &= \frac{\text{Conc} - (\text{Conc}_{\text{low}} + \text{Conc}_{\text{high}})/2}{(\text{Conc}_{\text{high}} - \text{Conc}_{\text{low}})/2} \\ &= \frac{\text{Conc} - 20}{5} \\ &= \begin{cases} 1 & \text{if Conc}=25 \\ -1 & \text{if Conc}=15 \end{cases}\end{aligned}$$

$$\begin{aligned}x_2 &= \frac{\text{Catalyst} - (\text{Catalyst}_{\text{low}} + \text{Catalyst}_{\text{high}})/2}{(\text{Catalyst}_{\text{high}} - \text{Catalyst}_{\text{low}})/2} \\ &= \frac{\text{Catalyst} - 1.5}{0.5} \\ &= \begin{cases} 1 & \text{if Catalyst}=2 \\ -1 & \text{if Catalyst}=1 \end{cases}\end{aligned}$$

Regression model

Regression model fitting in R

```
# Define the data
y <- c(28, 25, 27, 36, 32, 32, 18, 19, 23, 31, 30, 29)
A <- rep(c(15, 25), each = 3, times = 2)
B <- rep(c(1, 2), each = 6)

# Create the data frame and compute coded variables
dat <- data.frame(A = A, B = B, y = y) |>
  transform(
    A_coded = (A - mean(A)) / abs(diff(range(A)) / 2),
    B_coded = (B - mean(B)) / abs(diff(range(B)) / 2)
  )

print(head(dat))
```

```
   A B  y A_coded B_coded
1 15 1 28     -1     -1
2 15 1 25     -1     -1
3 15 1 27     -1     -1
4 25 2 36      1      1
5 25 2 32      1      1
6 25 2 32      1      1
7 18 1 18     -1     -1
8 19 2 19      1      1
9 23 2 23      1      1
10 31 1 31      1      1
11 30 2 30      1      1
12 29 1 29     -1     -1
```

Regression model

Regression model fitting in R

```
fit <- lm(y ~ A_coded + B_coded, data = dat)
coef(fit)
```

(Intercept)	A_coded	B_coded
27.500000	4.166667	-2.500000

Regression model

The fitted regression model is

$$\hat{y} = 27.5 + 4.167x_1 - 2.5x_2$$

$$\hat{y} = 27.5 + \left(\frac{8.33}{2}\right)x_1 + \left(\frac{-5.00}{2}\right)x_2$$

If you look carefully:

- Intercept is the grand average of all 12 observations
- $\hat{\beta}_1$ and $\hat{\beta}_2$ are one-half the corresponding factor effect estimates

Ques:

Why is the regression coefficients are one half the effect estimates?

Answer:

Regression coefficient measures the effect of one-unit change in x on y , whereas effect estimate is based on a two-unit change (from -1 to $+1$)

Regression model

```
anova(lm(y ~ A_coded + B_coded, data = dat))
```

Analysis of Variance Table

Response: y

	Df	Sum Sq	Mean Sq	F value	Pr(>F)	
A_coded	1	208.333	208.333	47.269	7.265e-05	***
B_coded	1	75.000	75.000	17.017	0.002578	**
Residuals	9	39.667	4.407			

Signif. codes: 0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1

```
anova(lm(y ~ A_coded * B_coded, data = dat))
```

Analysis of Variance Table

Response: y

	Df	Sum Sq	Mean Sq	F value	Pr(>F)	
A_coded	1	208.333	208.333	53.1915	8.444e-05	***
B_coded	1	75.000	75.000	19.1489	0.002362	**
A_coded:B_coded	1	8.333	8.333	2.1277	0.182776	
Residuals	8	31.333	3.917			

Signif. codes: 0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1

Residuals and Model Adequacy

- The regression model can be used to obtain the predicted or fitted value of y at the four points in the design.
- Residuals, $e = y - \hat{y}$, are:

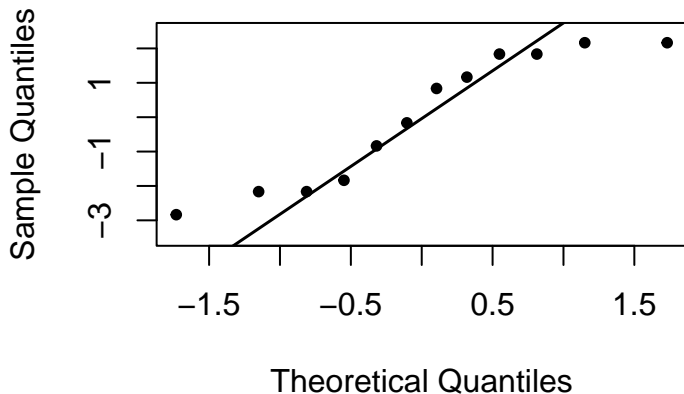
```
x1 <- dat$A_coded
x2 <- dat$B_coded
yhat <- 27.5 + (8.33/2)*x1 + (-5/2)*x2
resd <- y - yhat
resd
```

```
[1] 2.165 -0.835 1.165 1.835 -2.165 -2.165 -2.835 -1.835
[11] 0.835 -0.165
```

Residuals and Model Adequacy

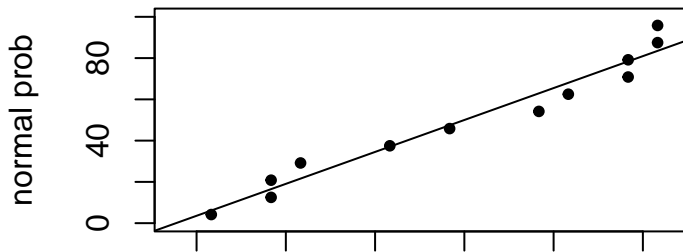
```
qqnorm(resd, pch=20, ylim=c(-3.5, 2.5))  
qqline(resd, lwd=1.5)
```

Normal Q-Q Plot



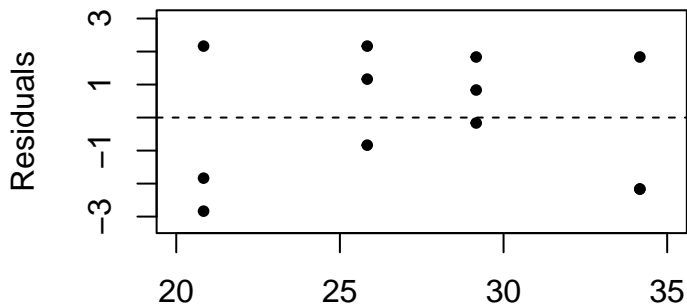
Residuals and Model Adequacy

```
rresd <- sort(resd)
j <- 100*(1:12-.5)/12
plot(rresd,j, pch=20, xlab="residual", ylab="normal prob",
      ylim=c(0,100), xlim=c(-3.25, 2.25))
abline(lm(j~rresd))
```



Residuals and Model Adequacy

```
plot(yhat, resid, xlab="Fitted", pch=20,  
     ylab="Residuals", ylim=c(-3.25, 3), xlim=c(20, 35))  
abline(h=0, lty=2)
```



Response surface and contour plot

The regression model

$$\hat{y} = 27.5 + \left(\frac{8.33}{2}\right)x_1 + \left(\frac{-5.00}{2}\right)x_2$$

can be used generate response surface plots.

It is desirable to construct such plots on the natural factor levels than the coded factor levels, so

$$\begin{aligned}\hat{y} &= 27.5 + \left(\frac{8.33}{2}\right)\left(\frac{\text{Conc} - 20}{5}\right) + \left(\frac{-5.00}{2}\right)\left(\frac{\text{Catalyst} - 1.5}{0.5}\right) \\ &= 18.33 + 0.833 \text{ Conc} - 5.00 \text{ Catalyst}\end{aligned}$$

Response surface and contour plot

```
res <- lm(y~A+B, data=dat)
res
```

Call:

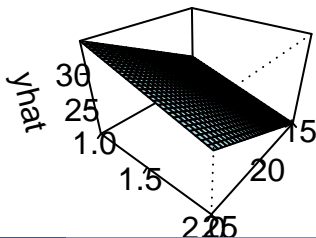
```
lm(formula = y ~ A + B, data = dat)
```

Coefficients:

(Intercept)	A	B
18.3333	0.8333	-5.0000

Response surface and contour plot

```
conc <- seq(15, 25, length=30)
cata <- seq(1, 2, length=30)
yhatn <- outer(conc, cata, function(x, y) 18.33 + .833*x - 5*y)
persp(conc, cata, yhatn, theta=130, phi=30, expand=.7,
      zlab="\n\nyhat", xlab="", ylab="", nticks=3,
      col="lightblue", ticktype="detailed")
```



Response surface and contour plot

```
contour(conc, cata, yhatn, nlevels=6, xlab="concentration",  
        ylab="catalyst")
```


Example

A router is used to cut registration notches in printed circuit boards. The average notch dimension is satisfactory, but there is too much variability in the process. This excess variability leads to problems in board assembly. A quality control team assigned to this project decided to use a designed experiment to study the process. The team considered two factors: bit size (A) and speed (B).

Two levels were chosen for each factor (bit size A at $1/16$ inch and $1/8$ inch and speed B at 40 rpm and 80 rpm and a 2^2 design was set up. Four boards were tested at each of the four runs in the experiment, and the resulting data are shown in the following table:

Example

<i>Run</i>		<i>A</i>	<i>B</i>	<i>Vibration</i>				<i>Total</i>
1	(1)	-	-	18.2	18.9	12.9	14.4	64.4
2	<i>a</i>	+	-	27.2	24.0	22.4	22.5	96.1
3	<i>b</i>	-	+	15.9	14.5	15.1	14.2	59.7
4	<i>ab</i>	+	+	41.0	43.9	36.3	39.9	161.1

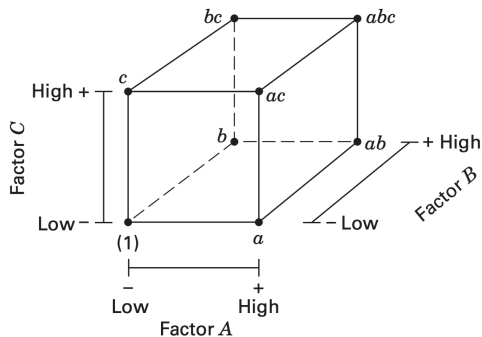
- Compute the main effects and interaction effect.
- Compute the sum of squares associated with the effects.
- Construct the ANOVA table and draw conclusion.
- Find residuals using regression method.

Subsection 3

6.3 The 2^3 design

6.3 The 2^3 design

The 2^3 **factorial design** has three factors (say A , B , and C) and each factor has two levels each. The design has 8 treatment combinations.



(a) Geometric view

Run	Factor		
	A	B	C
1	-	-	-
2	+	-	-
3	-	+	-
4	+	+	-
5	-	-	+
6	+	-	+
7	-	+	+
8	+	+	+

(b) Design matrix

6.3 The 2^3 design

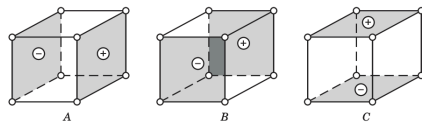
- Standard order $\rightarrow (1), a, b, ab, c, ac, bc,$ and abc .
 - ▶ Remember that these symbols also represent the *total* of all n observations taken at that particular treatment combination.
- Three different notations for 2^3 design:

Run	A	B	C	Labels	A	B	C
1	-	-	-	(1)	0	0	0
2	+	-	-	<i>a</i>	1	0	0
3	-	+	-	<i>b</i>	0	1	0
4	+	+	-	<i>ab</i>	1	1	0
5	-	-	+	<i>c</i>	0	0	1
6	+	-	+	<i>ac</i>	1	0	1
7	-	+	+	<i>bc</i>	0	1	1
8	+	+	+	<i>abc</i>	1	1	1

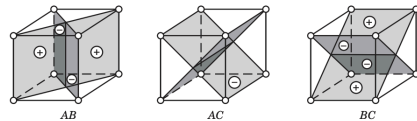
Effects in the 2^3 design

- Main effects: A , B , and C
- Two-factor interactions: AB , AC , BC
- Three-factor interaction: ABC

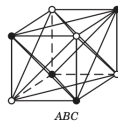
Effects in the 2^3 design



(a) Main effects



(b) Two-factor interaction



(c) Three-factor interaction

● = + runs
○ = - runs

Effects in the 2^3 design

The A effect is just the average of the four runs where A is at the high level (\bar{y}_{A^+}) minus the average of the four runs where A is at the low level (\bar{y}_{A^-}),

$$\begin{aligned} A &= \bar{y}_{A^+} - \bar{y}_{A^-} \\ &= \frac{a + ab + ac + abc}{4n} - \frac{(1) + b + c + bc}{4n} \end{aligned}$$

This equation can be rearranged as

$$A = \frac{1}{4n} [a + ab + ac + abc - (1) - b - c - bc]$$

Similarly

$$B = \frac{1}{4n} [b + ab + bc + abc - (1) - a - c - ac]$$

$$C = \frac{1}{4n} [c + ac + bc + abc - (1) - a - b - ab]$$

The quantities in brackets are **contrasts** in the treatment combinations

Effects in the 2^3 design

Construction of plus and minus table:

- 1 Signs for the main effects are determined by associating a plus with the high level and a minus with the low level.
- 2 Once the signs for the main effects have been established, the signs for the remaining columns can be obtained by multiplying the appropriate preceding columns

Effects in the 2^3 design

Interesting properties of *Table of plus and minus signs*:

- 1 Except the column I , every column has an equal number of $+$ and $-$ signs
- 2 The sum of the products of any two columns is zero
- 3 The column I multiplied any column leaves the column unchanged, column I is known as identity column
- 4 Product of any two columns yields a column in the table, e.g. $A \times B = AB$, $AB \times BC = AB^2C = AC \pmod{2}$.

Exponents in the products are formed by using **modulus 2** arithmetic.

Property-2 indicates that it is an **Orthogonal** design

Sum of squares

In the 2^3 design with n replicates, the sum of squares for any effect is

$$SS = \frac{\text{Contrast}^2}{2^3 n} = \frac{\text{Contrast}^2}{8n}$$

The 2^3 design: An example

A soft drink bottler is interested in obtaining more uniform fill heights in the bottles produced his manufacturing process.

The filling machine theoretically fills fills each bottle to the correct target height, but in practice, there is variation around this target.

The bottler would like to understand better the sources of variability and eventually reduce it.

The process engineer can control three factors during the filling process: *percentage of carbonation* (A), *operating pressure* (B), and *line speed* (C).

Each factor has two levels: A (10% and 12%), B (25 psi and 30 psi), and C (200 b/min and 300 b/min).

The 2^3 design: An example

The data:

Run	coded factor			fill height deviation	
	A	B	C	rep I	rep II
1	-1	-1	-1	-3	-1
2	1	-1	-1	0	1
3	-1	1	-1	-1	0
4	1	1	-1	2	3
5	-1	-1	1	-1	0
6	1	-1	1	2	1
7	-1	1	1	1	1
8	1	1	1	6	5

Notation for the response: y_{ijkl} , $i, j, k, l = 1, 2$

The 2^3 design: An example

Run	coded factor			fill height deviation		Total	comb.
	A	B	C	rep I	rep II		
1	-1	-1	-1	-3	-1	-4	(1)
2	1	-1	-1	0	1	1	a
3	-1	1	-1	-1	0	-1	b
4	1	1	-1	2	3	5	ab
5	-1	-1	1	-1	0	-1	c
6	1	-1	1	2	1	3	ac
7	-1	1	1	1	1	2	bc
8	1	1	1	6	5	11	abc

Estimation of effects

Main effect of A

$$\begin{aligned}A &= (abc + ab + ac + a - bc - b - c - (1))/4n \\&= (11 + 5 + 3 + 1 - 2 + 1 + 1 + 4)/8 \\&= 24/8 \\&= 3\end{aligned}$$

Similarly,

$$B = (abc + ab + bc + b - ac - a - c - (1))/4n = 2.25$$

$$C = (abc + ac + bc + c - ab - a - b - (1))/4n = 1.75$$

Estimation of effects

Interactions

$$AB = (abc + ab + c + (1) - ac - bc - a - b)/4n = 0.75$$

$$AC = (abc + ac + b + (1) - ab - bc - a - c)/4n = 0.25$$

$$BC = (abc + bc + a + (1) - ab - ac - b - c)/4n = 0.5$$

$$ABC = (abc + a + b + c - ab - ac - bc - (1))/4n = 0.5$$

Sum of squares

$$SS_A = \frac{\text{Contrast}_A^2}{8n} = \frac{24^2}{16} = 36$$

$$SS_{AB} = \frac{6^2}{16} = 2.25$$

$$SS_B = \frac{18^2}{16} = 20.25$$

$$SS_{AC} = \frac{2^2}{16} = 0.25$$

$$SS_C = \frac{14^2}{16} = 12.25$$

$$SS_{BC} = \frac{4^2}{16} = 1$$

$$SS_{ABC} = \frac{4^2}{16} = 1$$

Sum of squares

Factor	Effect estimate	Sum of squares	Percentage contribution
A	3	36	46.154
B	2.25	20.25	25.962
C	1.75	12.25	15.705
AB	0.75	2.25	2.885
AC	0.25	0.25	0.321
BC	0.5	1	1.282
ABC	0.5	1	1.282
Error		5	
Total		78	

Percentage contribution is a rough but effective guide to the relative importance of each model term. Main effects dominate the process accounting for over 87 percent of the total variation.

Analysis of variance table

Source of variation	Sum of squares	Degrees of freedom	Mean square	F_0	$\Pr(F_0 > F)$
A	36	1	36	57.6	0
B	20.25	1	20.25	32.4	0
C	12.25	1	12.25	19.6	0
AB	2.25	1	2.25	3.6	0.094
AC	0.25	1	0.25	0.4	0.545
BC	1	1	1	1.6	0.242
ABC	1	1	1	1.6	0.242
Error	5	8	0.625		
Total	78	15			

All the main effects are highly significant and only the interaction between carbonation and pressure is significant at about 10 percent level of significance.

Regression model

The fitted regression model for the design is

$$\begin{aligned}\hat{y} &= 1 + \left(\frac{3}{2}\right)x_A + \left(\frac{2.25}{2}\right)x_B + \left(\frac{1.75}{2}\right)x_C + \left(\frac{0.75}{2}\right)x_Ax_B \\ &= 1 + \left(\frac{3}{2}\right)\frac{\text{carb} - 11}{1.0} + \left(\frac{2.25}{2}\right)\frac{\text{pres} - 27.5}{2.5} + \left(\frac{1.75}{2}\right)\frac{\text{speed} - 250}{50} \\ &\quad + \left(\frac{0.75}{2}\right)\left(\frac{\text{carb} - 11}{1.0}\right)\left(\frac{\text{pres} - 27.5}{2.5}\right)\end{aligned}$$

$$\hat{y} = 9.625 + 2.62\text{carb} - 1.20\text{pres} + 0.035\text{speed} + 0.38\text{carb} \times \text{speed}$$

Regression model

The model sum of squares is

$$SS_{\text{Model}} = SS_A + SS_B + SS_C + SS_{AB} + SS_{AC} + SS_{BC} + SS_{ABC}$$

Thus the statistic

$$F_0 = \frac{MS_{\text{Model}}}{MS_E}$$

is testing the hypotheses

$$H_0 : \beta_1 = \beta_2 = \beta_3 = \beta_{12} = \beta_{13} = \beta_{23} = \beta_{123} = 0$$

$$H_1 : \text{at least one } \beta \neq 0$$

If F_0 is large, we would conclude that at least one variable has a nonzero effect. Then each individual factorial effect is tested for significance using the F statistic.

Regression model

$$R^2 = \frac{SS_{\text{Model}}}{SS_{\text{Total}}}$$

It measures the proportion of total variability explained by the model.

A potential problem with this statistic is that it always increases as factors are added to the model, even if these factors are not significant. The adjusted R^2 statistic, defined as

$$R_{\text{Adj}}^2 = 1 - \frac{SS_E / df_E}{SS_{\text{Total}} / df_{\text{Total}}}$$

Regression model

R_{Adj}^2 is a statistic that is adjusted for the “size” of the model, that is, the number of factors.

The adjusted R^2 can actually decrease if nonsignificant terms are added to a model. The standard error of each coefficient, defined as

$$se(\hat{\beta}) = \sqrt{V(\hat{\beta})} = \sqrt{\frac{MS_E}{n2^k}} = \sqrt{\frac{MS_E}{N}}$$

Regression model

The 95 percent confidence intervals on each regression coefficient are computed from

$$\hat{\beta} - t_{0.025, N-p} \text{se}(\hat{\beta}) \leq \beta \leq \hat{\beta} + t_{0.025, N-p} \text{se}(\hat{\beta})$$

where the degrees of freedom on t are the number of degrees of freedom for error; that is, N is the total number of runs in the experiment (16), and p is the number of model parameters (8).

Other Methods for Judging the Significance of Effects.

The analysis of variance is a formal way to determine which factor effects are nonzero. Several other methods are useful. Now, we show how to calculate the standard error of the effects, and we use these standard errors to construct confidence intervals on the effects.

Confidence Interval of the Effect:

The $100(1 - \alpha)$ percent confidence intervals on the effects are computed from

$$\text{Effect} \pm t_{\alpha/2, N-p} * \text{se}(\text{Effect}),$$

where

$$\text{se}(\text{Effect}) = \frac{2S}{\sqrt{n2^k}}, \quad \text{where } S^2 = MS_E$$

Regression analysis with R

```
# Define the response variable
y3 <- c(-3, 0, -1, 2, -1, 2, 1, 6,
        -1, 1, 0, 3, 0, 1, 1, 5)

# Create treatment variables
xA <- rep(c(-1, 1), each = 1, times = 8)
xB <- rep(c(-1, 1), each = 2, times = 4)
xC <- rep(c(-1, 1), each = 4, times = 2)

# Fit the linear model
reg.y3 <- lm(y3 ~ xA + xB + xC + xA:xB)
coef(reg.y3)
```

(Intercept)	xA	xB	xC	xA:xB
1.000	1.500	1.125	0.875	0.375

Regression analysis with R

```
anova(reg.y3)
```

Analysis of Variance Table

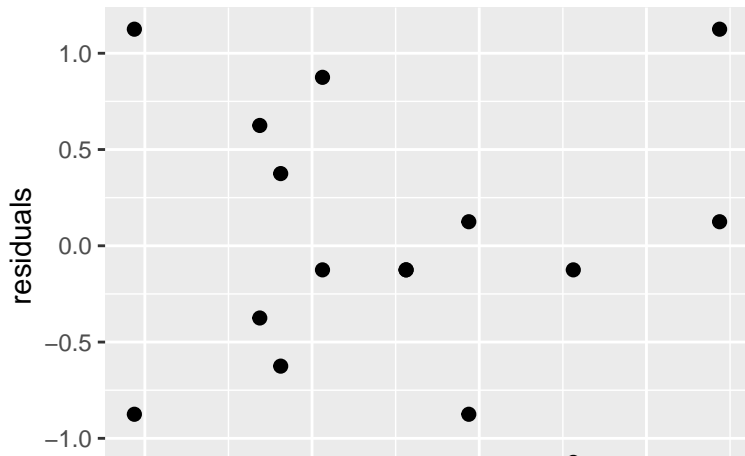
Response: y3

	Df	Sum Sq	Mean Sq	F value	Pr(>F)	
xA	1	36.00	36.000	54.6207	1.376e-05	***
xB	1	20.25	20.250	30.7241	0.0001746	***
xC	1	12.25	12.250	18.5862	0.0012327	**
xA:xB	1	2.25	2.250	3.4138	0.0916999	.
Residuals	11	7.25	0.659			

Signif. codes: 0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1

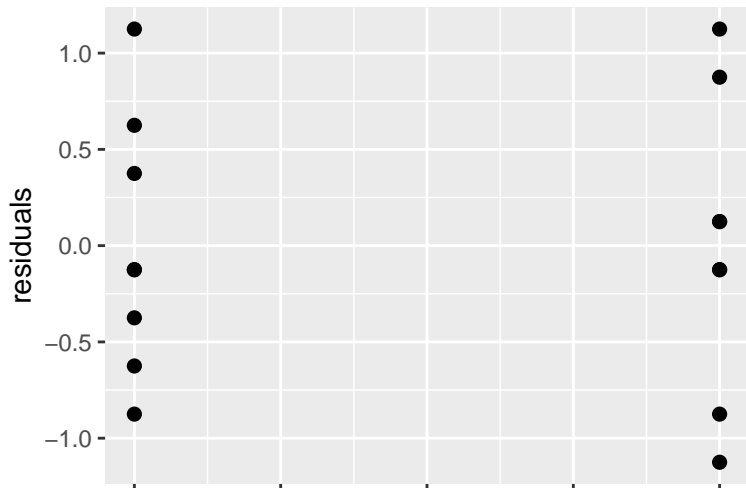
Residual analysis

```
library(broom)
ggplot(augment(reg.y3)) +
  geom_point(aes(.fitted, .resid), size = 2) +
  labs(x = "fitted", y = "residuals")
```



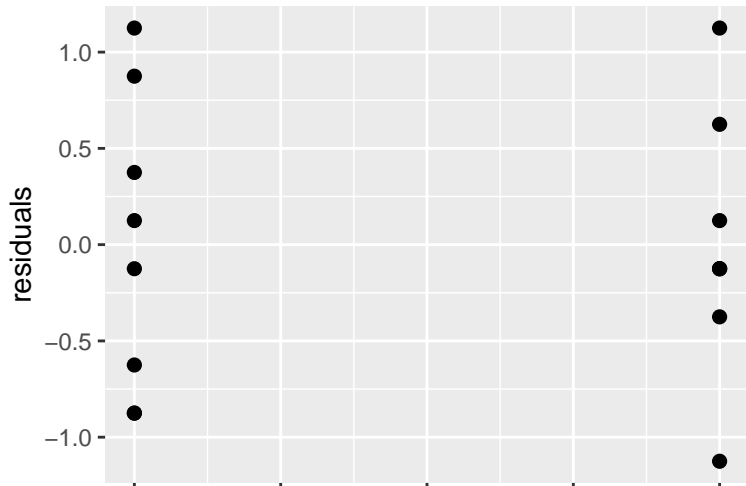
Residual analysis

```
ggplot(augment(reg.y3)) +  
  geom_point(aes(xA, .resid), size = 2) +  
  labs(x = "Carbonation", y = "residuals")
```



Residual analysis

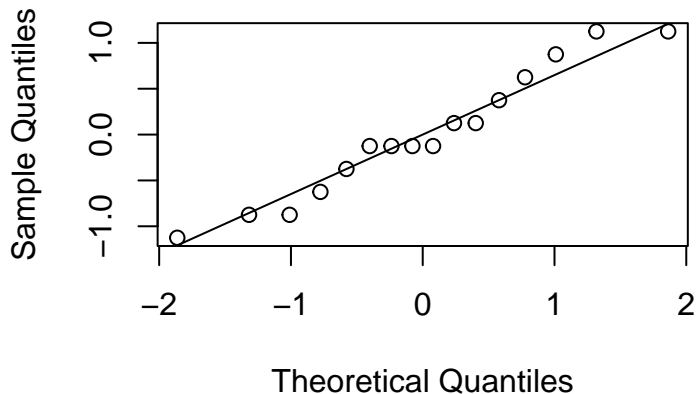
```
ggplot(augment(reg.y3)) +  
  geom_point(aes(xB, .resid), size = 2) +  
  labs(x = "Pressure", y = "residuals")
```



Residual analysis

```
qqnorm(residuals(reg.y3))  
qqline(residuals(reg.y3))
```

Normal Q-Q Plot



Full model vs our model

```
dat2 <- data.frame(y=y3, x1=xA, x2=xB, x3=xC)
head(dat2)
```

	y	x1	x2	x3
1	-3	-1	-1	-1
2	0	1	-1	-1
3	-1	-1	1	-1
4	2	1	1	-1
5	-1	-1	-1	1
6	2	1	-1	1

Full model vs our model

```
res2 <- lm(y~xA*xB*xC, data=dat2)
anova(res2)
```

Analysis of Variance Table

Response: y

	Df	Sum Sq	Mean Sq	F value	Pr(>F)	
xA	1	36.00	36.000	57.6	6.368e-05	***
xB	1	20.25	20.250	32.4	0.0004585	***
xC	1	12.25	12.250	19.6	0.0022053	**
xA:xB	1	2.25	2.250	3.6	0.0943498	.
xA:xC	1	0.25	0.250	0.4	0.5447373	
xB:xC	1	1.00	1.000	1.6	0.2415040	
xA:xB:xC	1	1.00	1.000	1.6	0.2415040	
Residuals	8	5.00	0.625			

Signif. codes: 0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1

Full model vs our model

```
res3 <- lm(y~xA+xB+xC+xA:xB, data=dat2)
anova(res3)
```

Analysis of Variance Table

Response: y

	Df	Sum Sq	Mean Sq	F value	Pr(>F)	
xA	1	36.00	36.000	54.6207	1.376e-05	***
xB	1	20.25	20.250	30.7241	0.0001746	***
xC	1	12.25	12.250	18.5862	0.0012327	**
xA:xB	1	2.25	2.250	3.4138	0.0916999	.
Residuals	11	7.25	0.659			

Signif. codes: 0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1

Full model vs our model

```
anova(res3, res2)
```

Analysis of Variance Table

Model 1: $y \sim xA + xB + xC + xA:xB$

Model 2: $y \sim xA * xB * xC$

	Res.Df	RSS	Df	Sum of Sq	F	Pr(>F)
1	11	7.25				
2	8	5.00	3	2.25	1.2	0.37

Subsection 4

6.4 The general 2^k design

The general 2^k design

- The 2^k factorial design is a design with k factors each has two levels.
- A statistical model for 2^k design would include
 - ▶ k main effects
 - ▶ $\binom{k}{2}$ two-factor interactions
 - ▶ $\binom{k}{3}$ three-factor interactions
 - ▶ ...
 - ▶ one k -factor interaction
- For a 2^k design, the complete model would contain $2^k - 1$ effects
- The treatment combinations can be written in a standard order, e.g.

(1) $a b ab c ac bc abc d ad \dots$

The general 2^k design

- The complete model for 2^k design with n replications has
 - ▶ $n2^k - 1$ total degrees of freedom
 - ▶ $(n2^k - 1) - (2^k - 1) = 2^k(n - 1)$ error degrees of freedom
- For a 2^k design, contrast for the effect $AB \cdots K$ can be expressed as

$$\text{Contrast}_{AB\dots} = (a \pm 1)(b \pm 1) \cdots (k \pm 1)$$

- ▶ ordinary algebra is used with “1” being replaced by (1) in the final expression.
 - ▶ The sign in each set of parentheses is negative if the factor is included in the effect and positive if the factor is not included.
- E.g. for a 2^2 design, the contrast

$$A = (a - 1)(b + 1) = ab + a - b - (1)$$

$$AB = (a - 1)(b - 1) = ab - a - b + (1)$$

The general 2^k design

- Estimate of the contrast

$$AB \dots K = \frac{2}{n2^k} [\text{Contrast}_{AB \dots K}]$$

- Sums of squares

$$SS_{AB \dots K} = \frac{1}{n2^k} [\text{Contrast}_{AB \dots K}]^2,$$

where n is the number of replications.

The general 2^k design

■ TABLE 6.9

Analysis of Variance for a 2^k Design

Source of Variation	Sum of Squares	Degrees of Freedom
<i>k</i> main effects		
<i>A</i>	SS_A	1
<i>B</i>	SS_B	1
⋮	⋮	⋮
<i>K</i>	SS_K	1
$\binom{k}{2}$ two-factor interactions		
<i>AB</i>	SS_{AB}	1
<i>AC</i>	SS_{AC}	1
⋮	⋮	⋮
<i>JK</i>	SS_{JK}	1
$\binom{k}{3}$ three-factor interactions		
<i>ABC</i>	SS_{ABC}	1
<i>ABD</i>	SS_{ABD}	1
⋮	⋮	⋮
<i>IJK</i>	SS_{IJK}	1
⋮	⋮	⋮
$\binom{k}{k}$ <i>k</i> -factor interaction		
<i>ABC ⋯ K</i>	$SS_{ABC \cdots K}$	1
Error	SS_E	$2^k(n - 1)$
Total	SS_T	$n2^k - 1$

The general 2^k design

■ TABLE 6.8

Analysis Procedure for a 2^k Design

1. Estimate factor effects
 2. Form initial model
 - a. If the design is replicated, fit the full model
 - b. If there is no replication, form the model using a normal probability plot of the effects
 3. Perform statistical testing
 4. Refine model
 5. Analyze residuals
 6. Interpret results
-

Subsection 5

6.5 A single replicate of the 2^k design

6.5 A single replicate of the 2^k design

- Total number of treatment combinations in a 2^k factorial design could be very large even for a moderate number of factors
- For example, a 2^5 design has 32 treatment combinations, a 2^6 design has 64 treatment combinations, and so on
- In many practical situations, the available resources may only allow a single replicate of the design to be run
- Single replicate may cause problem if the response is highly variable
- A single replicate of a 2^k design is sometime called an **unreplicated factorial**

6.5 A single replicate of the 2^k design

- With only one replicate, pure error cannot be estimated, so commonly used analysis of variance cannot be performed
- Two approaches are commonly used for analysing unreplicated factorial design
- ① Consider certain high-order interactions as negligible and combine their mean squares to estimate the error.
 - ▶ This approach is based on the assumption that the most systems is dominated by some of the main effects and low-order interactions, and most of the high-order interactions are negligible (**sparsity of effects principle**)

6.5 A single replicate of the 2^k design

- ② Higher-order interactions could be of interest, in that case polling higher-order interactions to estimate the error variance is not appropriate.
 - ▶ In such case, **normal probability plots** of the effect estimates could be of help. The negligible effects should be normally distributed with mean 0 and variance σ^2 and will fall in a straight line on the plot. On the other hand, significant effects will have nonzero means and will not lie along the straight line.

6.5 A single replicate of the 2^k design

EXAMPLE 6.2

A chemical product is produced in a pressure vessel. A factorial experiment is carried out in the pilot plant to study the factors thought to influence the **filtration rate** of this product.

Four factors **temperature** (A), **pressure** (B), **concentration of formaldehyde** (C), and **stirring rate** (D) are thought to be important for the chemical product.

The design matrix and the response data obtained from a single replicate of the 2^4 experiment are shown in Table 6.10.

6.5 A single replicate of the 2^k design

■ TABLE 6.10

Pilot Plant Filtration Rate Experiment

Run Number	Factor				Run Label	Filtration Rate (gal/h)
	A	B	C	D		
1	-	-	-	-	(1)	45
2	+	-	-	-	<i>a</i>	71
3	-	+	-	-	<i>b</i>	48
4	+	+	-	-	<i>ab</i>	65
5	-	-	+	-	<i>c</i>	68
6	+	-	+	-	<i>ac</i>	60
7	-	+	+	-	<i>bc</i>	80
8	+	+	+	-	<i>abc</i>	65
9	-	-	-	+	<i>d</i>	43
10	+	-	-	+	<i>ad</i>	100
11	-	+	-	+	<i>bd</i>	45
12	+	+	-	+	<i>abd</i>	104
13	-	-	+	+	<i>cd</i>	75
14	+	-	+	+	<i>acd</i>	86
15	-	+	+	+	<i>bcd</i>	70
16	+	+	+	+	<i>abcd</i>	96

6.5 A single replicate of the 2^k design

- We will begin the analysis of these data by constructing a normal probability plot of the effect estimates.
 - ▶ The table of plus and minus signs for the contrast constants for the 2^4 design are shown in Table 6.11.
 - ▶ From these contrasts, we may estimate the 15 factorial effects and the sums of squares shown in Table 6.12.

6.5 A single replicate of the 2^k design

■ **TABLE 6.11**

Contrast Constants for the 2^4 Design

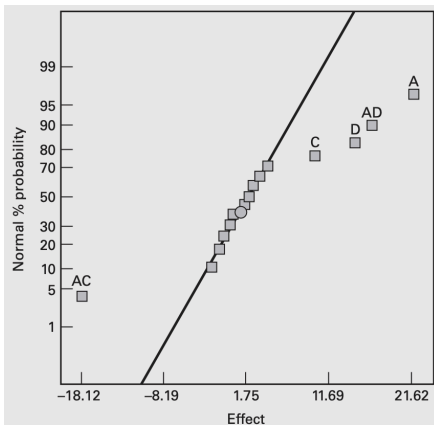
	<i>A</i>	<i>B</i>	<i>AB</i>	<i>C</i>	<i>AC</i>	<i>BC</i>	<i>ABC</i>	<i>D</i>	<i>AD</i>	<i>BD</i>	<i>ABD</i>	<i>CD</i>	<i>ACD</i>	<i>BCD</i>	<i>ABCD</i>
(1)	-	-	+	-	+	+	-	-	+	+	-	+	-	-	+
<i>a</i>	+	-	-	-	-	+	+	-	-	+	+	+	+	-	-
<i>b</i>	-	+	-	-	+	-	+	-	+	-	+	+	-	+	-
<i>ab</i>	+	+	+	-	-	-	-	-	-	-	-	+	+	+	+
<i>c</i>	-	-	+	+	-	-	+	-	+	+	-	-	+	+	-
<i>ac</i>	+	-	-	+	+	-	-	-	-	+	+	-	-	+	+
<i>bc</i>	-	+	-	+	-	+	-	-	+	-	+	-	+	-	+
<i>abc</i>	+	+	+	+	+	+	+	-	-	-	-	-	-	-	-
<i>d</i>	-	-	+	-	+	+	-	+	-	-	+	-	+	+	-
<i>ad</i>	+	-	-	-	-	+	+	+	+	-	-	-	-	+	+
<i>bd</i>	-	+	-	-	+	-	+	+	-	+	-	-	+	-	+
<i>abd</i>	+	+	+	-	-	-	-	+	+	+	+	+	-	-	-
<i>cd</i>	-	-	+	+	-	-	+	+	-	-	+	+	-	-	+
<i>acd</i>	+	-	-	+	+	-	-	+	+	-	-	+	+	-	-
<i>bcd</i>	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-
<i>abcd</i>	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+

6.5 A single replicate of the 2^k design

■ **TABLE 6.12**

Factor Effect Estimates and Sums of Squares for the 2^4 Factorial in Example 6.2

Model Term	Effect Estimate	Sum of Squares	Percent Contribution
A	21.625	1870.56	32.6397
B	3.125	39.0625	0.681608
C	9.875	390.062	6.80626
D	14.625	855.563	14.9288
AB	0.125	0.0625	0.00109057
AC	-18.125	1314.06	22.9293
AD	16.625	1105.56	19.2911
BC	2.375	22.5625	0.393696
BD	-0.375	0.5625	0.00981515
CD	-1.125	5.0625	0.0883363
ABC	1.875	14.0625	0.245379
ABD	4.125	68.0625	1.18763
ACD	-1.625	10.5625	0.184307
BCD	-2.625	27.5625	0.480942
ABCD	1.375	7.5625	0.131959



■ **FIGURE 6.11** Normal probability plot of the effects for the 2^4 factorial in Example 6.2

6.5 A single replicate of the 2^k design

```
df <- data.frame(  
  y = c(45, 71, 48, 65, 68, 60, 80, 65, 43, 100, 45, 104, 75,  
  A = rep(c(-1, 1), times = 8),  
  B = rep(c(-1, 1), each = 2, times = 4),  
  C = rep(c(-1, 1), each = 4, times = 2),  
  D = rep(c(-1, 1), each = 8)  
)  
model <- lm(y ~ A * B * C * D, data = df)  
dat6b <- tibble(  
  `Model terms` = c('A', 'B', 'C', 'D', 'AB', 'AC', 'BC',  
                    'AD', 'BD', 'CD', 'ABC', 'ABD',  
                    'ACD', 'BCD', 'ABCD'),  
  `Effect estimates` = coef(model)[-1] * 2,  
  SS = anova(model)$"Sum Sq"[1:15],  
  `Percentage contribution` = 100 * (SS / sum(SS))  
)
```

6.5 A single replicate of the 2^k design

```
kableExtra::kable(dat6b, digits = 3, align = 'c')
```

Model terms	Effect estimates	SS	Percentage contribution
A	21.625	1870.562	32.640
B	3.125	39.062	0.682
C	9.875	390.063	6.806
D	14.625	855.563	14.929
AB	0.125	0.062	0.001
AC	-18.125	1314.062	22.929
BC	2.375	22.562	0.394
AD	16.625	1105.562	19.291
BD	-0.375	0.563	0.010
CD	-1.125	5.063	0.088
ABC	1.875	14.063	0.245
ABD	4.125	68.062	1.188
ACD	-1.625	10.563	0.184
BCD	-2.625	27.563	0.481
ABCD	1.375	7.563	0.132

6.5 A single replicate of the 2^k design

- The important effects that emerge from this analysis are
 - ▶ the main effects of A , C , and D and
 - ▶ the AC and AD interactions.

6.5 A single replicate of the 2^k design

```
library(ggDoE)
main_effects(df, response='y', exclude_vars = c('B'),
             color_palette = 'viridis', n_columns=3)
```

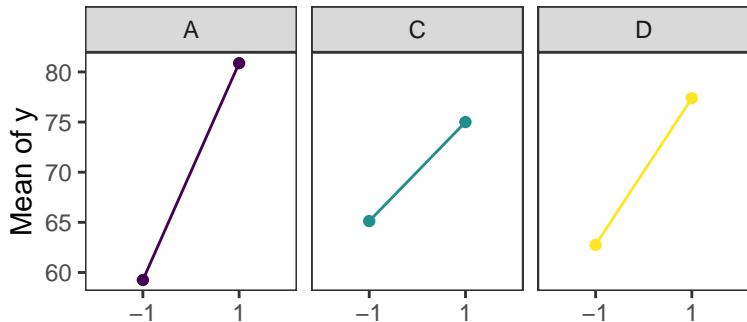


Figure 1: Main effect plots

6.5 A single replicate of the 2^k design

- The main effects of A, C, and D are plotted in Figure. All three effects are positive, and if we considered only these main effects, we would run all three factors at the high level to maximize the filtration rate.
- However, it is always necessary to examine any interactions that are important. Remember that main effects do not have much meaning when they are involved in significant interactions.

6.5 A single replicate of the 2^k design

```
p1=interaction_effects(df, response='y',exclude_vars=c('B','D'))
p2=interaction_effects(df, response='y',exclude_vars=c('B','C'))
gridExtra::grid.arrange(p1, p2, ncol = 2)
```

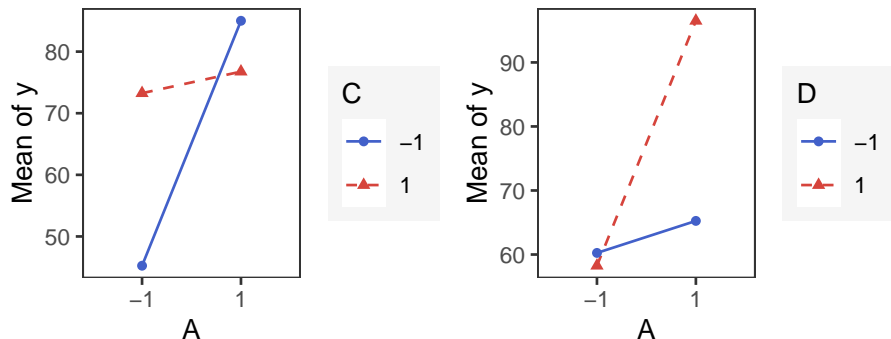


Figure 2: Interaction plots

6.5 A single replicate of the 2^k design

The AC interaction indicates: the A effect is very small when the C is at the high level and very large when the C is at the low level, with the best results obtained with low C and high A .

The AD interaction indicates: D has little effect at low A but a large positive effect at high A .

Therefore, the best filtration rates would appear to be obtained when A and D are at the high level and C is at the low level. This would allow the reduction of the formaldehyde concentration to a lower level, another objective of the experimenter.

Design projection

- Another interpretation of the effects in Figure 6.11 is possible
- Because B (pressure) is not significant and all interactions involving B are negligible, we may discard B from the experiment so that the design becomes a 2^3 factorial in A , C , and D with two replicates.
- This is easily seen from examining only columns A , C , and D in the design matrix shown in Table 6.10 and noting that those columns form two replicates of a 2^3 design.

Design projection

■ TABLE 6.10

Pilot Plant Filtration Rate Experiment

Run Number	Factor				Run Label	Filtration Rate (gal/h)
	A	B	C	D		
1	-	-	-	-	(1)	45
2	+	-	-	-	<i>a</i>	71
3	-	+	-	-	<i>b</i>	48
4	+	+	-	-	<i>ab</i>	65
5	-	-	+	-	<i>c</i>	68
6	+	-	+	-	<i>ac</i>	60
7	-	+	+	-	<i>bc</i>	80
8	+	+	+	-	<i>abc</i>	65
9	-	-	-	+	<i>d</i>	43
10	+	-	-	+	<i>ad</i>	100
11	-	+	-	+	<i>bd</i>	45
12	+	+	-	+	<i>abd</i>	104
13	-	-	+	+	<i>cd</i>	75
14	+	-	+	+	<i>acd</i>	86
15	-	+	+	+	<i>bcd</i>	70
16	+	+	+	+	<i>abcd</i>	96

Design projection

The analysis of variance for the data using this simplifying assumption is summarized in Table 6.13.

The conclusions that we would draw from this analysis are essentially unchanged from those of Example 6.2.

Note that by projecting the single replicate of the 2^4 into a replicated 2^3 , we now have both an estimate of the *ACD* interaction and an estimate of error based on what is sometimes called **hidden replication**

In general, if we have a single replicate of a 2^k design, and if h ($h < k$) factors are negligible and can be dropped, then the original data correspond to a full two-level factorial in the remaining $k - h$ factors with 2^h replicates.

Design projection

■ TABLE 6.13

Analysis of Variance for the Pilot Plant Filtration Rate Experiment in *A*, *C*, and *D*

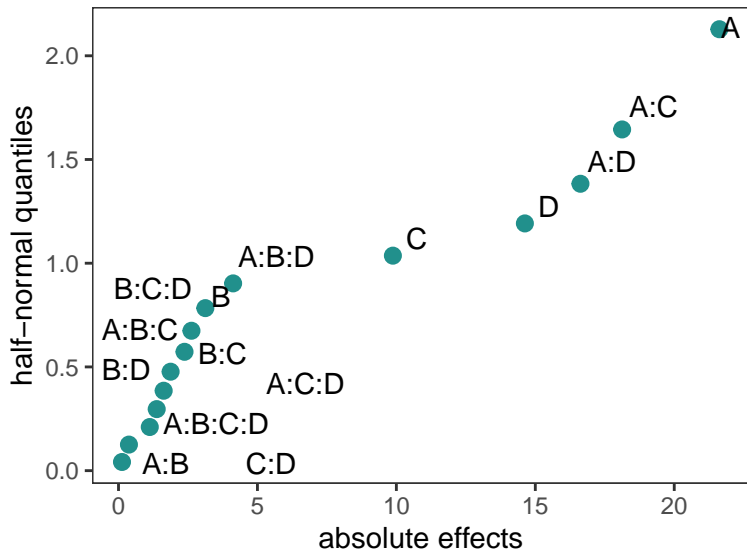
Source of Variation	Sum of Squares	Degrees of Freedom	Mean Square	F_0	<i>P</i> -Value
<i>A</i>	1870.56	1	1870.56	83.36	< 0.0001
<i>C</i>	390.06	1	390.06	17.38	< 0.0001
<i>D</i>	855.56	1	855.56	38.13	< 0.0001
<i>AC</i>	1314.06	1	1314.06	58.56	< 0.0001
<i>AD</i>	1105.56	1	1105.56	49.27	< 0.0001
<i>CD</i>	5.06	1	5.06	< 1	
<i>ACD</i>	10.56	1	10.56	< 1	
Error	179.52	8	22.44		
Total	5730.94	15			

The Half-Normal Plot of Effects

- An alternative to the normal probability plot of the factor effects is the half-normal plot.
- This is a plot of the absolute value of the effect estimates against their cumulative normal probabilities.
- The straight line on the half-normal plot always passes through the origin and should also pass close to the fiftieth percentile data value.

The Half-Normal Plot of Effects

```
ggDoE::half_normal(model)
```



Other Methods for Analyzing Unreplicated Factorials.

A widely used analysis procedure for an unreplicated two-level factorial design is the normal (or half-normal) plot of the estimated factor effects.

However, unreplicated designs are so widely used in practice that many formal analysis procedures have been proposed to overcome the subjectivity of the normal probability plot.

Hamada and Balakrishnan (1998) compared some of these methods.

- They found that the method proposed by **Lenth (1989)** has good power to detect significant effects. It is also easy to implement, and as a result it appears in several software packages for analyzing data from unreplicated factorials.

Subsection 6

6.6 Additional Examples of Unreplicated 2^k Designs

6.6 Additional Examples of Unreplicated 2^k Designs

EXAMPLE 6.3: Data Transformation in a Factorial Design

Subsection 7

6.7 2^k Designs are Optimal Designs

6.7 2^k Designs are Optimal Designs

The model parameter regression coefficients (and effect estimates) from a 2^k design are least squares estimates. For a 2^2 model, the regression model is

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2 + \varepsilon$$

The four observations from a 2^2 design:

$$(1) = \beta_0 + \beta_1(-1) + \beta_2(-1) + \beta_{12}(-1)(-1) + \varepsilon_1$$

$$a = \beta_0 + \beta_1(1) + \beta_2(-1) + \beta_{12}(1)(-1) + \varepsilon_2$$

$$b = \beta_0 + \beta_1(-1) + \beta_2(1) + \beta_{12}(-1)(1) + \varepsilon_3$$

$$ab = \beta_0 + \beta_1(1) + \beta_2(1) + \beta_{12}(1)(1) + \varepsilon_4$$

$$\mathbf{y} = \mathbf{X}\boldsymbol{\beta} + \boldsymbol{\varepsilon}, \mathbf{y} = \begin{bmatrix} (1) \\ a \\ b \\ ab \end{bmatrix}, \mathbf{X} = \begin{bmatrix} 1 & -1 & -1 & 1 \\ 1 & 1 & -1 & -1 \\ 1 & -1 & 1 & -1 \\ 1 & 1 & 1 & 1 \end{bmatrix}, \boldsymbol{\beta} = \begin{bmatrix} \beta_0 \\ \beta_1 \\ \beta_2 \\ \beta_{12} \end{bmatrix}, \boldsymbol{\varepsilon} = \begin{bmatrix} \varepsilon_1 \\ \varepsilon_2 \\ \varepsilon_3 \\ \varepsilon_4 \end{bmatrix}$$

6.7 2^k Designs are Optimal Designs

The least squares estimate of β is given by:

$$\hat{\beta} = (X'X)^{-1}X'y$$

Since this is an orthogonal design, the $X'X$ matrix is diagonal:

$$\hat{\beta} = \begin{bmatrix} 4 & 0 & 0 & 0 \\ 0 & 4 & 0 & 0 \\ 0 & 0 & 4 & 0 \\ 0 & 0 & 0 & 4 \end{bmatrix}^{-1} \begin{bmatrix} (1) + a + b + ab \\ a + ab - b - (1) \\ b + ab - a - (1) \\ (1) - a - b + ab \end{bmatrix}$$

6.7 2^k Designs are Optimal Designs

With this, we obtain:

$$\begin{bmatrix} \hat{\beta}_0 \\ \hat{\beta}_1 \\ \hat{\beta}_2 \\ \hat{\beta}_{12} \end{bmatrix} = \frac{1}{4} \mathbf{I}_4 \begin{bmatrix} (1) + a + b + ab \\ a + ab - b - (1) \\ b + ab - a - (1) \\ (1) - a - b + ab \end{bmatrix} = \begin{bmatrix} \frac{(1)+a+b+ab}{4} \\ \frac{a+ab-b-(1)}{4} \\ \frac{b+ab-a-(1)}{4} \\ \frac{(1)-a-b+ab}{4} \end{bmatrix}$$

- The **“usual” contrasts** are shown in the matrix of $X'y$.
- The $X'X$ **matrix is diagonal** as a consequence of the orthogonal design.
- The **regression coefficient estimates** are exactly half of the “usual” effect estimates.

6.7 2^k Designs are Optimal Designs

The matrix $(X'X)$ has some useful properties

$$\begin{aligned} V(\hat{\beta}) &= \sigma^2 (\text{diagonal element of } (X'X)^{-1}) \\ &= \frac{\sigma^2}{4} \quad \longrightarrow \quad \text{Minimum possible value for a four-run design} \end{aligned}$$

$$|X'X| = 256 \quad \longrightarrow \quad \text{Maximum possible value for a four-run design}$$

Notice that these results depend on both the design you have chosen and the model.

6.7 2^k Designs are Optimal Designs

It turns out that the volume of the joint confidence region that contains all the model regression coefficients is inversely proportional to the square root of the determinant of $X'X$.

Therefore, to make this joint confidence region as small as possible, we would want to choose a design that makes the determinant of $X'X$ as large as possible.

In general, a design that minimizes the variance of the model regression coefficients (or maximize the determinant of $X'X$) is called a ***D*-optimal design**.

The 2^k design is a *D*-optimal design for fitting the first-order model or the first-order model with interaction.

Subsection 8

6.8 The Addition of Center Points to the 2^k Design

6.8 The Addition of Center Points to the 2^k Design

A potential concern in the use of two-level factorial designs is the assumption of linearity in the factor effects.

First-order model (with interaction):

$$y = \beta_0 + \sum_{j=1}^k \beta_j x_j + \sum_{i < j} \beta_{ij} x_i x_j + \epsilon. \quad (6.28)$$

is capable of representing some curvature in the response function.

Second-order model:

$$y = \beta_0 + \sum_{j=1}^k \beta_j x_j + \sum_{i < j} \beta_{ij} x_i x_j + \sum_{j=1}^k \beta_{jj} x_j^2 + \epsilon \quad (6.29)$$

where β_{jj} represent pure **Second-order** or **quadratic effects**.

6.8 The Addition of Center Points to the 2^k Design

In running a two-level factorial experiment, we usually anticipate fitting the first-order model in Equation 6.28, but we should be alert to the possibility that the second-order model in Equation 6.29 is more appropriate.

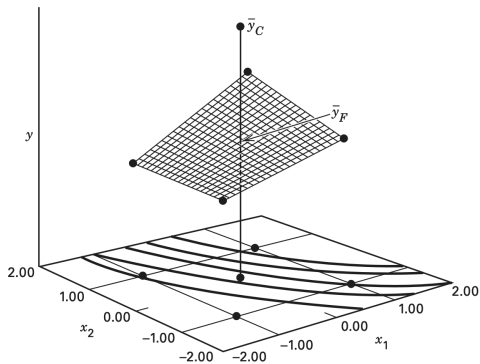
There is a method of replicating certain points in a 2^k factorial that will provide *protection against curvature from second-order effects* as well as allow *an independent estimate of error* to be obtained.

The method consists of adding **center points** to the 2^k design. These consist of n_C replicates run at the points $x_i = 0 (i = 1, 2, \dots, k)$.

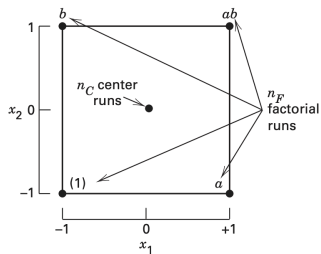
One important reason for adding the replicate runs at the design center is that center points do not affect the usual effect estimates in a 2^k design.

When we add center points, we assume that the k factors are **quantitative**.

6.8 The Addition of Center Points to the 2^k Design



■ FIGURE 6.37 A 2^2 design with center points



■ FIGURE 6.38 A 2^2 design with center points

6.8 The Addition of Center Points to the 2^k Design

Let \bar{y}_F be the average of the n_F runs at the four factorial points, and \bar{y}_C be the average of the n_C runs at the center point.

$\bar{y}_F = \bar{y}_C \rightarrow$ no “curvature”

$$H_0 : \sum_{j=1}^k \beta_{jj} = 0$$

$$H_1 : \sum_{j=1}^k \beta_{jj} \neq 0$$

$$SS_{\text{Pure quadratic}} = \frac{n_F n_C (\bar{y}_F - \bar{y}_C)^2}{n_F + n_C} \quad (6.30)$$

The sum of square has a single degree of freedom.

6.8 The Addition of Center Points to the 2^k Design

This sum of squares may be incorporated into the ANOVA and may be compared to the error mean square to test for pure quadratic curvature.

Furthermore, if the factorial points in the design are unreplicated, one may use the n_C center points to construct an estimate of error with $n_C - 1$ degrees of freedom.

Example 6.7 (Extended 6.2)

We will illustrate the addition of center points to a 2^k design by reconsidering the pilot plant experiment in Example 6.2.

Recall that this is an unreplicated 2^4 design.

Refer to the original experiment shown in Table 6.10.

Example 6.7 (Extended 6.2)

■ TABLE 6.10

Pilot Plant Filtration Rate Experiment

Run Number	Factor				Run Label	Filtration Rate (gal/h)
	A	B	C	D		
1	-	-	-	-	(1)	45
2	+	-	-	-	<i>a</i>	71
3	-	+	-	-	<i>b</i>	48
4	+	+	-	-	<i>ab</i>	65
5	-	-	+	-	<i>c</i>	68
6	+	-	+	-	<i>ac</i>	60
7	-	+	+	-	<i>bc</i>	80
8	+	+	+	-	<i>abc</i>	65
9	-	-	-	+	<i>d</i>	43
10	+	-	-	+	<i>ad</i>	100
11	-	+	-	+	<i>bd</i>	45
12	+	+	-	+	<i>abd</i>	104
13	-	-	+	+	<i>cd</i>	75
14	+	-	+	+	<i>acd</i>	86
15	-	+	+	+	<i>bcd</i>	70
16	+	+	+	+	<i>abcd</i>	96

Example 6.7 (Extended 6.2)

Suppose that four center points are added to this experiment, and at the points $x_1 = x_2 = x_3 = x_4 = 0$ the four observed filtration rates were 73, 75, 66, and 69.

- The average of these four center points is $\bar{y}_C = 70.75$
- The average of the 16 factorial runs is $\bar{y}_F = 70.06$.

Since \bar{y}_C and \bar{y}_F are very similar, we suspect that there is no strong curvature present.

Example 6.7 (Extended 6.2)

The mean square for **pure error** is calculated from the center points as follows:

$$\begin{aligned}MS_E &= \frac{SS_E}{n_C - 1} = \frac{\sum_{\text{Center points}} (y_i - \bar{y}_c)^2}{n_C - 1} \\ &= \frac{\sum_{i=1}^4 (y_i - 70.75)^2}{4 - 1} = 16.25\end{aligned}$$

Example 6.7 (Extended 6.2)

The difference $\bar{y}_F - \bar{y}_C = 70.06 - 70.75 = -0.69$ is used to compute the **pure quadratic** (curvature) sum of squares from Equation 6.30 as follows:

$$\begin{aligned}SS_{\text{Pure quadratic}} &= \frac{n_F n_C (\bar{y}_F - \bar{y}_C)^2}{n_F + n_C} \\ &= \frac{(16)(4)(-0.69)^2}{16 + 4} = 1.51\end{aligned}$$

Example 6.7 (Extended 6.2)

The upper portion of the Table 6.24 shows ANOVA for the full model.

ANOVA for the Full Model					
Source of Variation	Sum of Squares	DF	Mean Square	F	Prob > F
Model	5730.94	15	382.06	23.51	0.0121
A	1870.56	1	1870.56	115.11	0.0017
B	39.06	1	39.06	2.40	0.2188
C	390.06	1	390.06	24.00	0.0163
D	855.56	1	855.56	52.65	0.0054
AB	0.063	1	0.063	3.846E-003	0.9544
AC	1314.06	1	1314.06	80.87	0.0029
AD	1105.56	1	1105.56	68.03	0.0037
BC	22.56	1	22.56	1.39	0.3236
BD	0.56	1	0.56	0.035	0.8643
CD	5.06	1	5.06	0.31	0.6157
ABC	14.06	1	14.06	0.87	0.4209
ABD	68.06	1	68.06	4.19	0.1332
ACD	10.56	1	10.56	0.65	0.4791
BCD	27.56	1	27.56	1.70	0.2838
ABCD	7.56	1	7.56	0.47	0.5441
Pure quadratic					
Curvature	1.51	1	1.51	0.093	0.7802
Pure error	48.75	3	16.25		
Cor total	5781.20	19			

Example 6.7 (Extended 6.2)

The ANOVA indicates that there is no evidence of second-order curvature in the response over the region of exploration (p-value=0.7802).

That is, the null hypothesis $H_0 : \beta_{11} + \beta_{22} + \beta_{33} + \beta_{44} = 0$ cannot be rejected.

The significant effects are A, C, D, AC , and AD .

Example 6.7 (Extended 6.2)

The ANOVA for the reduced model is shown in the lower portion of Table 6.24.

Model	5535.81	5	1107.16	59.02	<0.000
A	1870.56	1	1870.56	99.71	<0.000
C	390.06	1	390.06	20.79	0.0005
D	855.56	1	855.56	45.61	<0.000
AC	1314.06	1	1314.06	70.05	<0.000
AD	1105.56	1	1105.56	58.93	<0.000
Pure quadratic					
curvature	1.51	1	1.51	0.081	0.7809
Residual	243.87	13	18.76		
Lack of fit	195.12	10	19.51	1.20	0.4942
Pure error	48.75	3	16.25		
Cor total	5781.20	19			

The results of this analysis agree with those from Example 6.2, where the important effects were isolated using the normal probability plotting method.